

COMPONENT SPECIFIC MODELING*

R.J. Maffeo, R.L. McKnight, M.T. Tipton, and G. Weber
General Electric Company

INTRODUCTION

The overall objective of this program is to develop and verify a series of interdisciplinary modeling and analysis techniques that have been specialized to address three specific hot section components. These techniques incorporate data as well as theoretical methods from many diverse areas including cycle and performance analysis, heat transfer analysis, linear and nonlinear stress analysis, and mission analysis. Building on the proven techniques already available in these fields, the new methods developed through this contract are integrated to provide an accurate, efficient, and unified approach to analyzing combustor burner liners, hollow air-cooled turbine blades, and air-cooled turbine vanes. For these components, the methods developed predict temperature, deformation, stress, and strain histories throughout a complete flight mission.

The base program for the component specific modeling effort is illustrated in Figure (1). Nine separate tasks were arranged into two parallel activities. The component specific structural modeling activity in Figure (2), was directed towards the development of the analytical techniques and methodology required in the analysis of complex hot section components. The component specific thermomechanical load mission modeling effort illustrated in Figure (3), provides for the development of approximate numerical models for engine cycle, aerodynamic, and heat transfer analyses of hot section components.

THERMODYNAMIC AND THERMOMECHANICAL MODELS

The Thermodynamic Engine Model (TDEM) and the Thermomechanical Load (TDLM) Model have been reported on extensively at previous HOST conferences. They have been installed on the NASA Lewis CRAY for over a year where they have been exercised by both GE and NASA personnel. Figures 4, 5 and 6 show representative pieces of input and output of these models. Figure 4 shows the input to the TDEM defining a specific mission. Figure 5 shows the output of the TDEM giving the engine parameters for a mission. This is then the input to the TDLM. Figure 6 shows a snapshot of a portion of the output of the TDLM for a combustor nugget showing the result of running the TDEM and TDLM to be local structural temperature and pressure loading on a component.

COMBUSTOR STRUCTURAL ANALYSIS

The emphasis in Phase I of this program has been on automating the COSMO procedure for the combustor liner. The COSMO procedure continues with the output

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of the TDLM being structured as a data file for use in the combustor component specific model. Figure 7 defines the recipe which generates the combustor structural model. Figure 8 is a snapshot of a typical run of the combustor model when it was in the checkout phase as a free-standing code. As indicated, the model contains a default set of recipe parameters, only changes to this list need be given. After the recipe parameters have been set, only 5 parameters need be specified to generate a 3D sector model of a combustor to perform a hot streak analysis. The first parameter (shown as the number of exhaust nozzles) is required to divide the 360° combustor into the proper number of sectors. The next parameter (shown as the no. of circumferential elements) is used by the analyst to split up the circumferential sector into a number of slices, NS, for the 3D elements. Next, depending on the number of slices selected, the analyst can bias these slices by specifying NS-1 percents (program calculates final bias to total 100%). In this case the biasing selected, starting at the hot streak, was 5%, 15%, and 30% with the final slice being 50%. This is all the information that is required to generate a 3D finite element model consisting of 20-noded isoparametric elements. In this case the model consists of 648 elements, 3192 nodes and has 768 element faces with pressure loading. Figures 9 and 10 are graphical depictions of this 3D model. The combustor then maps the temperatures and pressures from the TDLM onto this model and generates data files for the structural analysis.

COSMO SYSTEM

Figure 11 shows a flow chart of the overall COSMO system including the action positions of the adaptive controls developed in this program. This system includes a bandwidth optimizer which is necessary to make the automatic remeshing/mesh refinement activity possible. For the combustor, the following adaptive controls have been incorporated into the system (the numbers are consistent with Figure 11).

1. time increment
2. load increment
3. plasticity tolerances
4. creep tolerances
5. number of master region elements
6. number of slices
7. position of slices
8. row refinement
9. element refinement

The first four adaptive controls are a function of the structural code being used. For this system the code and the controls are those developed under, "3D Inelastic Analysis Methods for Hot Section Structures." The other adaptive controls are keyed from a decision grid as indicated in Figure 12. The gradients in normalized stress, total strain, plastic strain, and creep strain will be used to rank requirements.

REFERENCES

1. McKnight, R.L., "Component Specific Modeling - First Annual Status Report," NASA CR-174765, 1983.
2. McKnight, R.L., "Component Specific Modeling - Second Annual Status Report," NASA CR-174925, 1985.

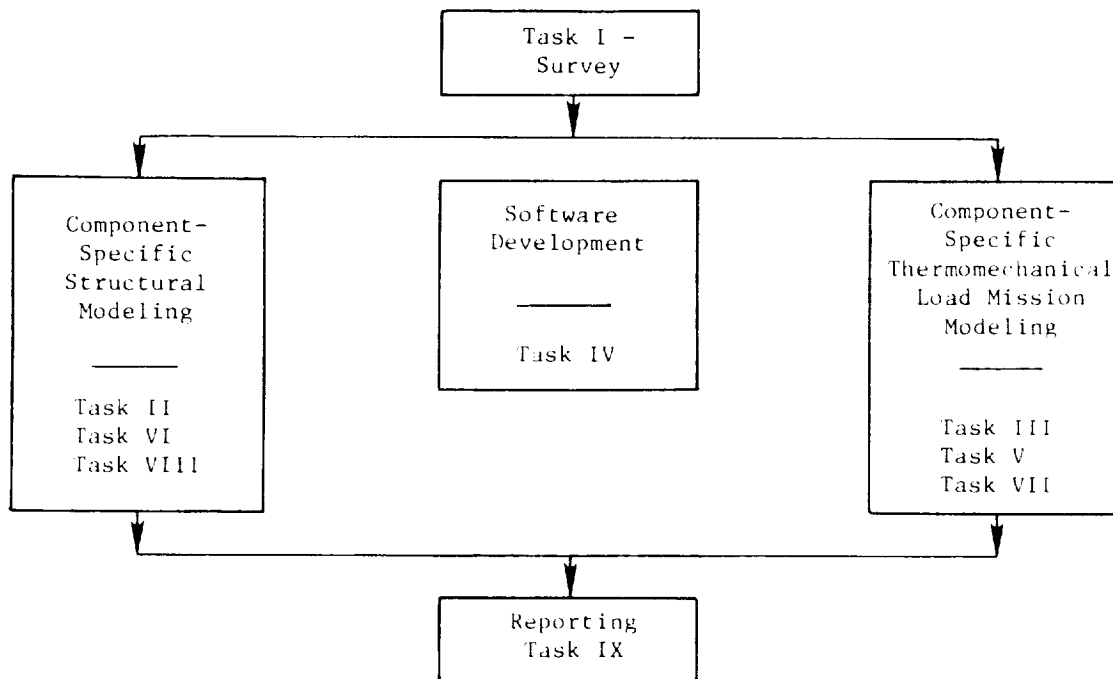


Figure 1. Component Specific Modeling Base Program.

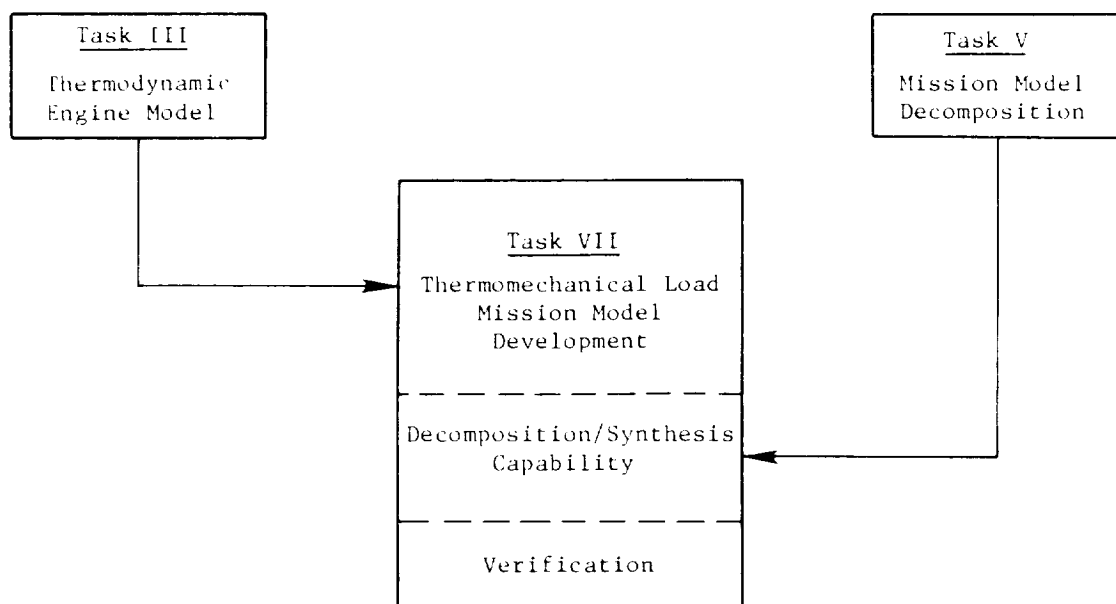


Figure 2. Component Specific Thermomechanical Load Mission Modeling.

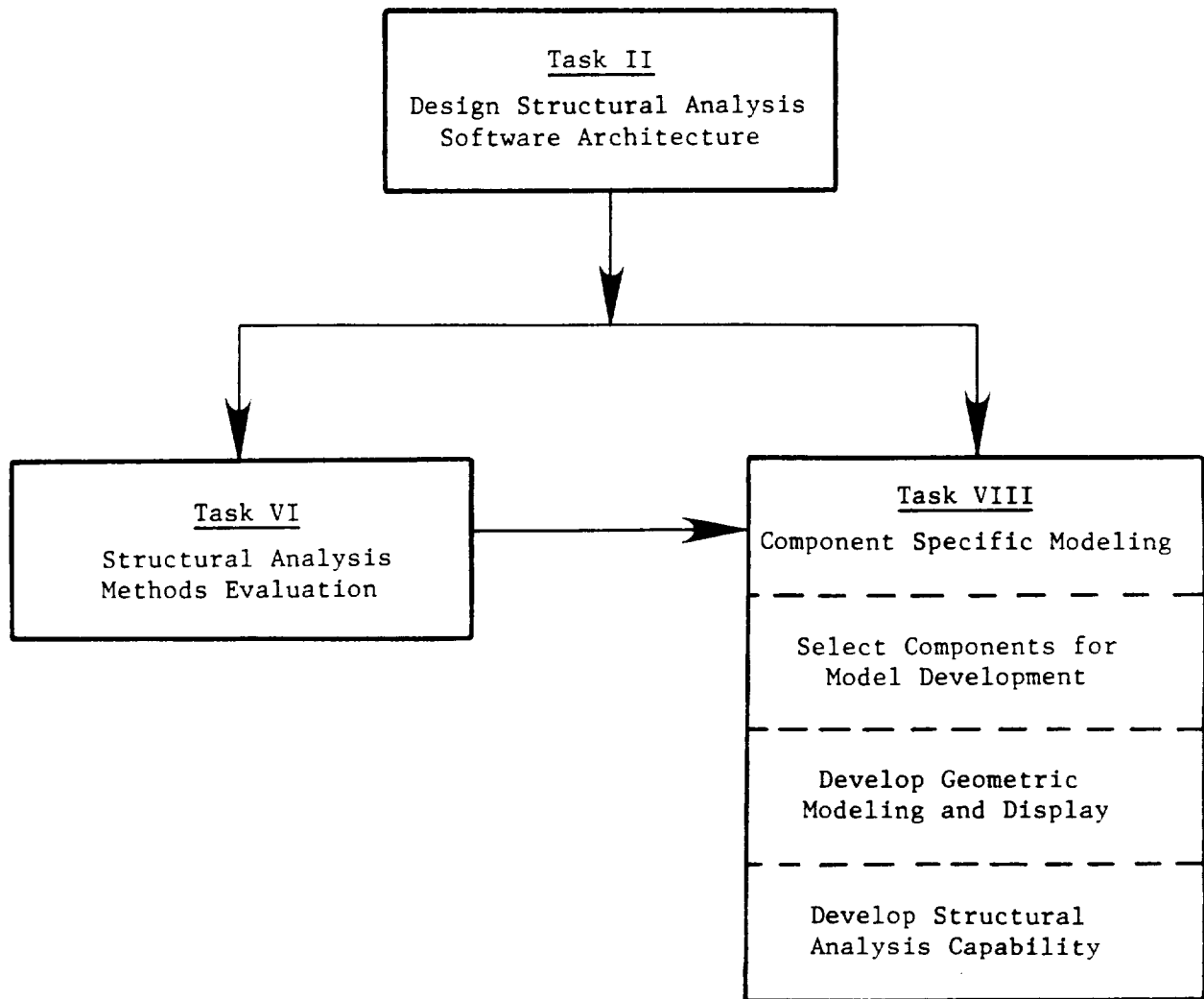


Figure 3. Component Specific Structural Modeling.

Case No.	Mach No.	Alt	Amb T	Code	ΔT_o	Power	Code	Fan Speed	Bleed Code	No. Offset Instr	Special Ref. Case	Flt Phase
197	0.00	0.	10	0.	41	0.	-1.	-1.	0	197	ST	
151	0.00	0.	10	0.	37	0.	-1.	-1.	0	0	GI1	
152	0.00	0.	10	0.	22	3730.	-1.	-1.	0	0	T01	
153	.243	2000.	10	0.	22	3743.	-1.	-1.	0	0	T02	
154	.243	2000.	10	0.	22	3634.	-1.	-1.	0	0	CL1	
155	.45	10000.	10	7.0	22	3634.	-1.	-1.	0	0	CL2	
156	.58	11000.	10	7.0	22	3618.	-1.	-1.	0	0	CL3	
157	.82	33000.	10	11.0	22	3724.	-1.	-1.	0	0	CL4	
158	.82	33000.	10	11.0	22	3466.	-1.	-1.	0	0	CRU	
159	.82	33000.	10	11.0	38	0.	-1.	-1.	0	0	D1	
160	.61	11000.	10	7.0	38	0.	-1.	-1.	0	0	D2	
161	.61	11000.	10	7.0	37	0.	-1.	-1.	0	0	D3	
162	.42	6000.	10	2.0	37	0.	-1.	-1.	0	0	D4	
163	.42	6000.	10	2.0	22	2798.	-1.	-1.	0	0	APPR	
164	.24	0.	10	0.0	22	2798.	-1.	-1.	0	0	LDG	
165	.18	0.	10	0.0	38	0.	-1.	-1.	0	0	FI	
166	.18	0.	10	0.0	39	2968.	-1.	-1.	0	0	TR1	
167	0.00	0.	10	0.0	39	2834.	-1.	-1.	0	0	TR2	

Figure 4. Inputs to Thermodynamic Engine Model.

DATE - 07/16/85

PHASE CASE #	* ENGINE PERFORMANCE DATA BY MISSION PHASE *										DTAMB	PHASE	
	P2	P25	P3	**	P4	ENGINE P4	P49	**	P5	P8			FNINI
1 197	14.696	14.696	14.696	14.696	14.696	0.	14.696	14.696	14.696	0.018	0.	0.	ST
2 151	14.696	15.531	73.295	73.295	69.860	0.	20.820	15.048	15.048	15.031	4538.261	0.	G11
3 151	14.696	15.531	73.295	73.295	69.860	0.	20.820	15.048	15.048	15.031	4538.261	0.	G11
4 152	14.696	32.353	422.356	422.356	402.822	0.	91.073	23.769	23.769	23.456	48907.753	0.	T01
5 153	14.238	31.569	413.413	413.413	394.295	0.	89.075	23.105	23.105	22.796	37628.904	0.	T02
6 154	14.237	30.207	388.387	388.387	370.358	0.	83.604	22.011	22.011	21.727	35094.032	0.	CL1
7 155	11.613	24.987	321.570	321.570	306.667	0.	69.312	17.822	17.822	17.580	24750.564	7.000	CL2
8 156	12.205	25.735	327.605	327.605	312.364	0.	70.500	18.211	18.211	17.966	22581.097	7.000	CL3
9 157	5.910	13.987	187.264	187.264	178.717	0.	40.557	10.415	10.415	10.275	11977.777	11.000	CL4
10 158	5.910	12.634	160.416	160.416	153.003	0.	34.522	8.872	8.872	8.752	9849.775	11.000	CRU
11 158	5.910	12.634	160.416	160.416	153.003	0.	34.522	8.872	8.752	8.752	9849.775	11.000	CRU
12 159	5.910	5.820	14.195	14.195	13.596	0.	5.152	3.878	3.878	3.876	-1602.839	11.000	D1
13 160	12.494	12.425	32.608	32.608	31.167	0.	12.205	9.855	9.855	9.850	-2438.477	7.000	D2
14 161	12.494	13.434	60.439	60.439	57.424	0.	15.634	10.153	10.153	10.136	-1434.762	7.000	D3
15 162	13.297	14.110	64.982	64.982	61.827	0.	17.506	12.153	12.153	12.137	-18.451	2.000	D4
16 163	13.296	19.957	205.245	205.245	195.282	0.	43.655	14.847	14.847	14.731	11991.389	2.000	APP
17 164	15.296	22.579	238.419	238.419	226.933	0.	51.135	17.924	17.924	17.793	16294.929	0.	L0G
18 165	15.032	15.290	42.036	42.036	40.353	0.	17.187	14.821	14.821	14.815	207.969	0.	F1
19 165	15.032	15.290	42.036	42.036	40.353	0.	17.187	14.821	14.815	14.815	207.969	0.	F1
20 166	15.033	23.122	261.537	261.537	249.111	0.	55.912	18.394	18.394	18.240	-11588.640	0.	TR1
21 167	14.697	21.554	234.321	234.321	223.144	0.	50.301	17.691	17.691	17.561	-4309.143	0.	TR2
22 151	14.696	15.531	73.295	73.295	69.860	0.	20.820	15.048	15.048	15.031	4538.261	0.	G11
23 151	14.696	15.531	73.295	73.295	69.860	0.	20.820	15.048	15.048	15.031	4538.261	0.	G11
24 197	14.696	14.696	14.696	14.696	14.696	0.	14.696	14.696	14.696	0.018	0.	0.	ST

Figure 5. Outputs From Thermodynamic Engine Model.

Pts 0.034 → 1.15 are Sufficient to Illustrate data

<u>X</u>	<u>Y</u>	<u>T_H</u>	<u>T_A</u>	<u>ΔT_H</u>	<u>ΔT_A</u>	<u>ΔP</u>
0.034	0.030	520.182	520.182	0.161	0.161	0.
0.094	0.030	521.284	521.284	0.263	0.263	0.
0.158	0.030	522.834	522.834	0.391	0.391	0.
0.208	0.030	523.901	523.901	0.463	0.463	0.
0.254	0.030	524.487	524.487	0.485	0.485	0.
0.288	0.030	524.935	524.935	0.499	0.499	0.
0.340	0.030	525.658	525.520	0.516	0.505	0.
0.404	0.030	526.519	526.002	0.523	0.489	0.
0.438	0.030	528.827	526.967	0.639	0.521	0.
0.584	0.040	530.446	527.690	0.735	0.562	0.
0.654	0.040	531.376	528.276	0.790	0.597	0.
0.764	0.040	531.686	528.758	1.032	0.800	0.
0.854	0.040	530.928	527.690	1.144	0.841	0.
0.934	0.044	529.826	527.311	1.310	1.014	0.
1.040	0.044	528.586	526.967	1.481	1.238	0.
1.074	0.040	527.828	526.726	1.461	1.284	0.
1.114	0.030	527.656	526.485	1.541	1.340	0.
1.150	0.030	527.518	526.381	1.613	1.405	0.

Figure 6. Outputs From Combustor Thermodynamic Loads Model.

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Combustor Liner Parameter List

Code	Name	Default	Code	Name	Default
1	X_1	0.0	2	Y_1	0.0
3	α_1	0.0	4	L_1	10.5
5	L_2	2.0	6	L_3	0.5
7	L_4	6.0	8	L_5	0.8
9	L_6	1.0	10	L_7	2.0
11	T_1	0.5	12	T_2	0.7
13	T_3	0.5	14	T_4	0.65
15	T_5	0.5	16	θ_1	90.0
17	θ_2	90.0	18	R_1	1.0
19	R_2	1.0	20	R_3	0.75
21	R_4	1.5	22	R_5	1.5
23	R_6	1.5			

X = Coordinate

Y = Coordinate

α = Angle wrt, x - Axis

L = Length

T = Thickness

θ = Angle of Rotation

R = Radius of Curvature

(n) = Parameter Code Number

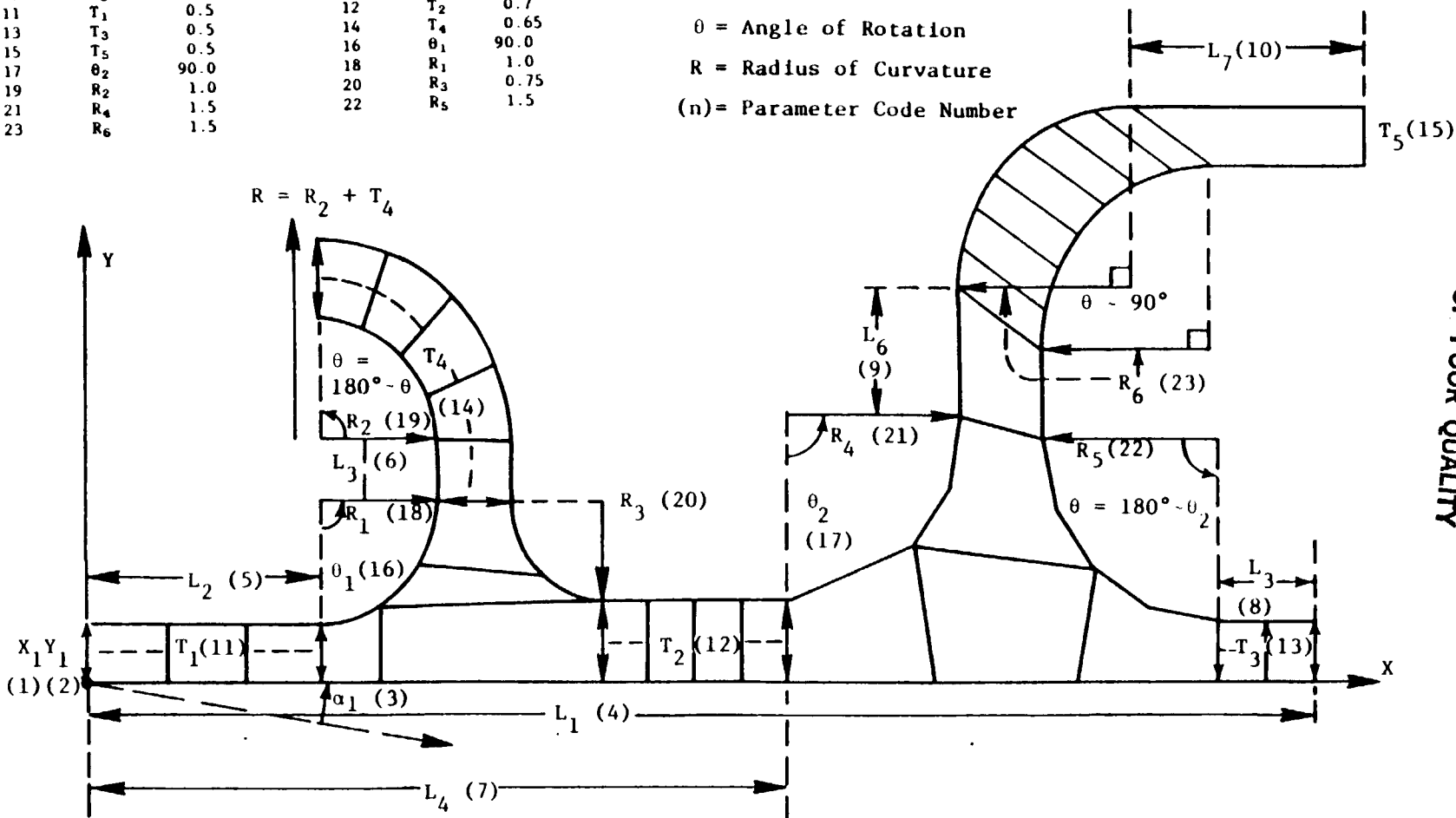


Figure 7. Combustor Liner Parameters.

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87RM /GM/MUGPRO

MUGGET RECIPE VERS.11 8/29/85

DO YOU MAKE A PARAMETER FILE 21? (0/1)

CODE	VALUE	CODE	VALUE
1	0.	2	0.
3	0.	4	1.16700
5	0.19200	6	0.04500
7	0.81000	8	0.06800
9	0.10000	10	0.20000
11	0.06000	12	0.08000
13	0.06000	14	0.06800
15	0.06800	16	110.00000
17	90.00000	18	0.06000
19	0.06700	20	0.12000
21	0.12500	22	0.08300
23	0.09500		

ENTER PARAMETER CHANGES (ENTRY CODE, NEW VALUE)
WHEN DONE ENTER 0 0

0 0

CODE	VALUE	CODE	VALUE
1	0.	2	0.
3	0.	4	1.16700
5	0.19200	6	0.04500
7	0.81000	8	0.06800
9	0.10000	10	0.20000
11	0.06000	12	0.08000
13	0.06000	14	0.06800
15	0.06800	16	110.00000
17	90.00000	18	0.06000
19	0.06700	20	0.12000
21	0.12500	22	0.08300
23	0.09500		

DO YOU WANT TO CHANGE PARAMETERS? (0/1)

READING FILE MUGCON

READING DONE

27 ELEMENTS READ

ENTER ENGINE TEMPERATURE AND PRESSURE FILE NAME

--GM/MUGINF

READING FILE /GM/MUGINF

READING DONE

36 CENTROIDS READ

ENTER THE NUMBER OF EXHAUST NOZZLES
AND THE NO. OF CIRCUMFERENTIAL ELEMENTS
BETWEEN T-AVE AND T-HOT (MAX NO.=10)

03 4

ENTER THE 3 CIRCUMFERENTIAL BIASING PARAMETERS

-- ENTER AS PERCENTS, THE SUM BEING LESS THAN 100% --

05 15 30

3192 NODES IN 3-D MODEL
648 ELEMENTS IN 3-D MODEL
768 FACES WITH PRESSURES

2-D NODE FILE IS TEMP FILE 20
PARAMETER FILE IS TEMP FILE 21
3-D UIF FILE IS TEMP FILE 26

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FIGURE 8. TYPICAL PROGRAM RUN

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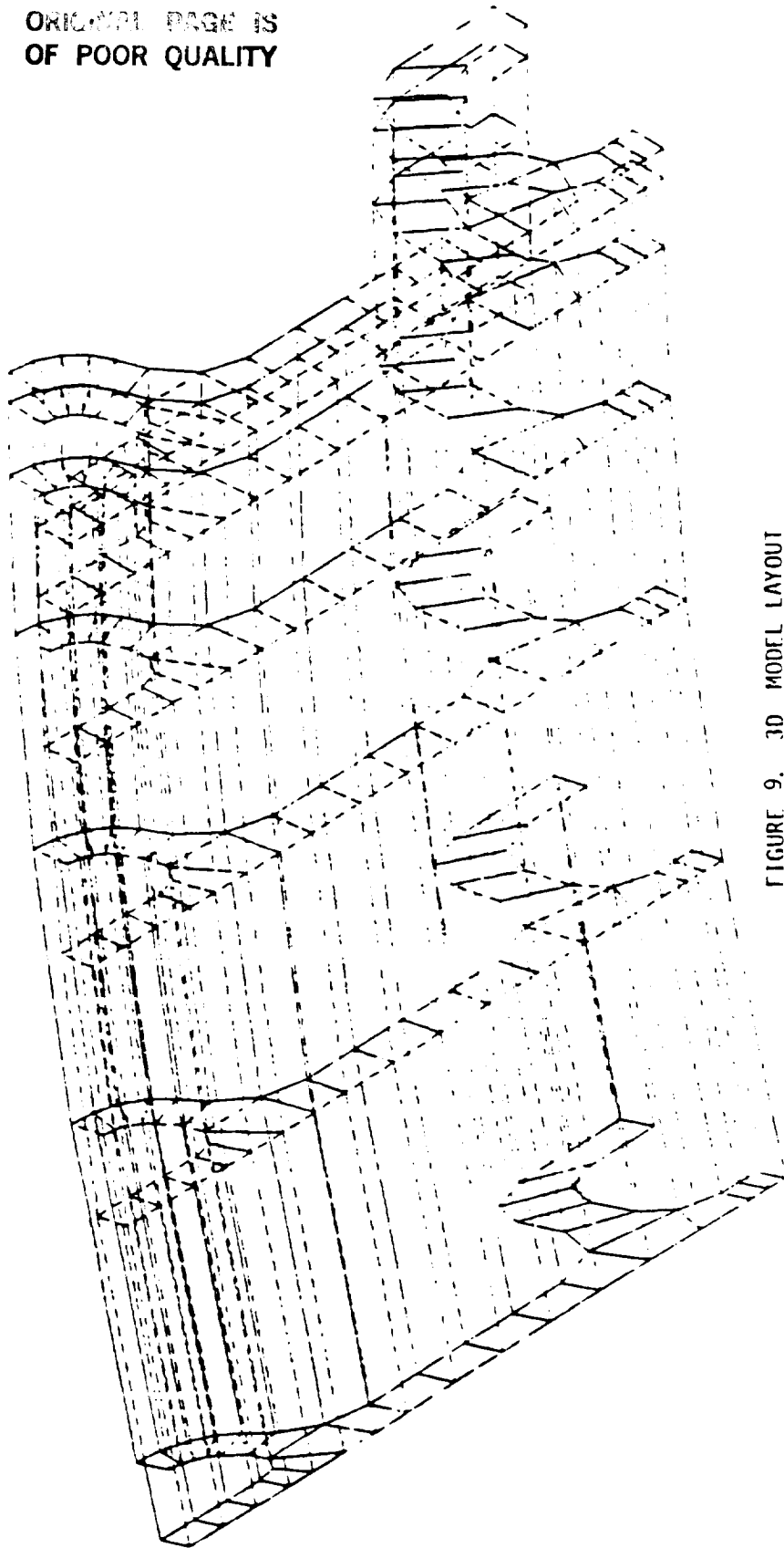
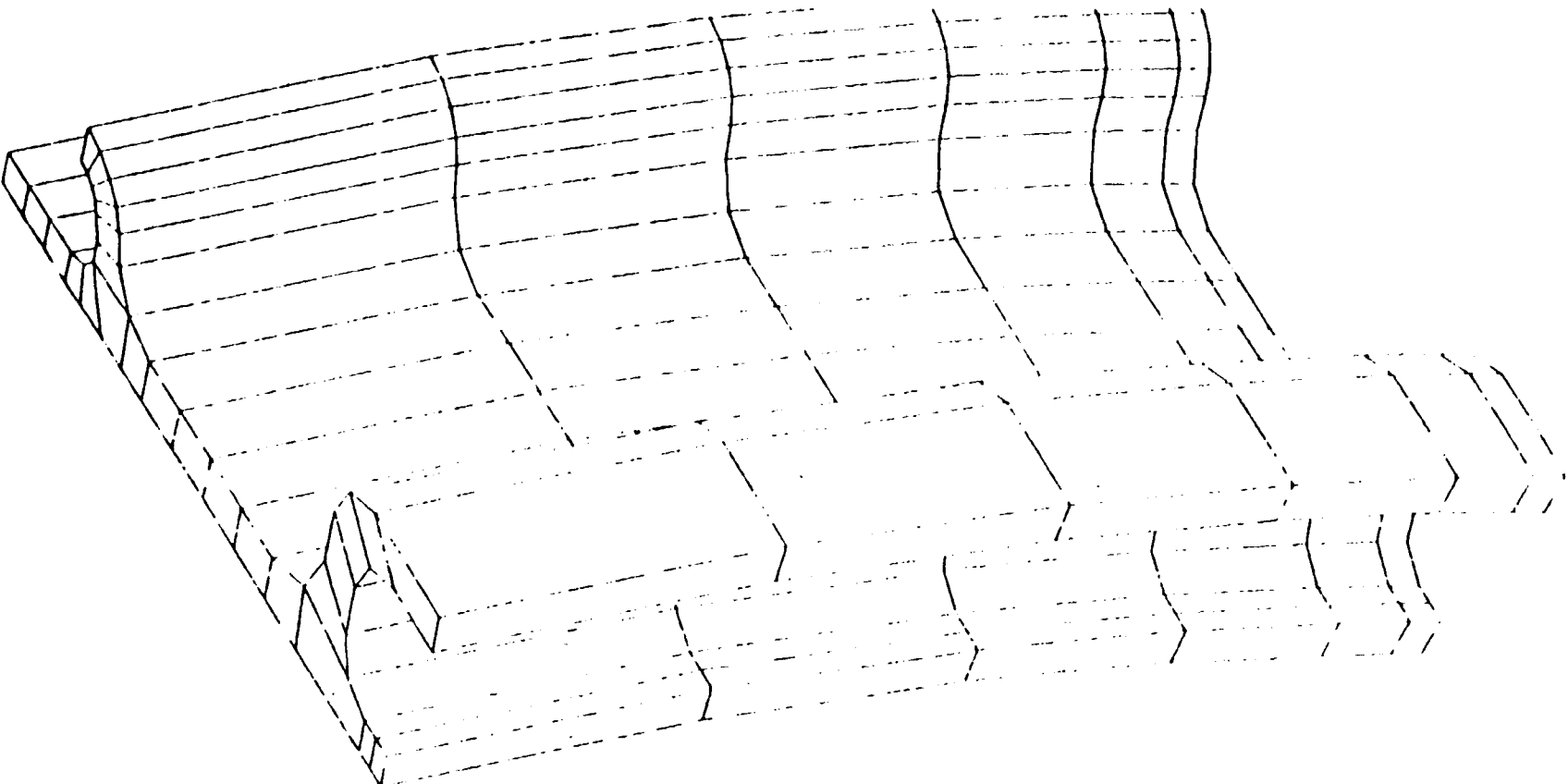


FIGURE 9. 3D MODEL LAYOUT

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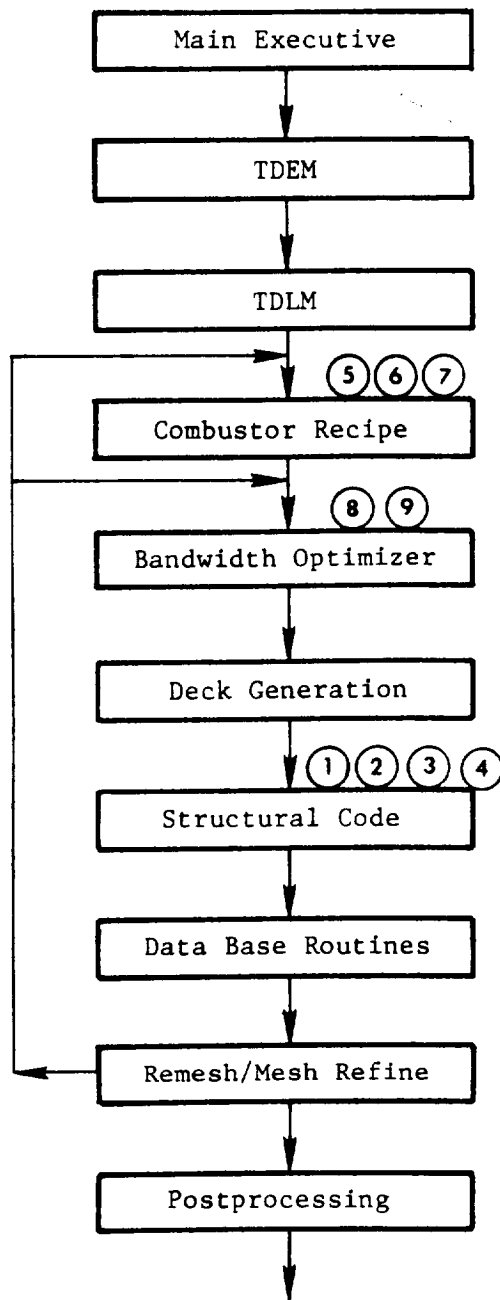


Figure 11. System Flow Chart Showing Adaptive Control Positions.

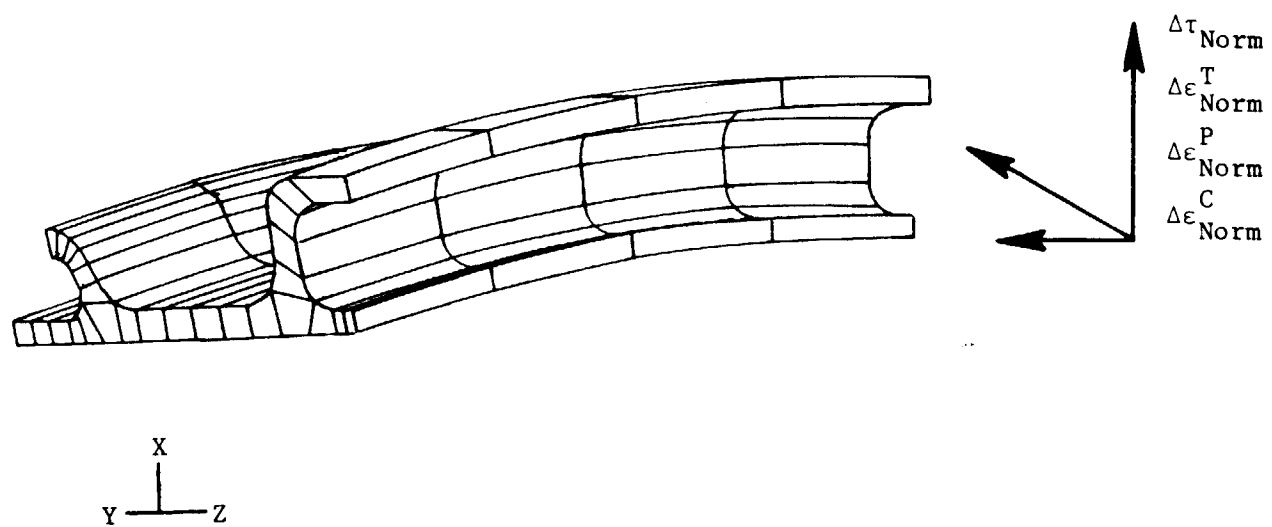


Figure 12. Combustor Nugget Decision Grid.